



## Less than 24 hours left

### What! Christmas is past already?

I cannot believe how quickly this year has gone by. Someone asked where my Christmas ("holiday season" for those who worry about such things) sale was. Well, to be honest, I had thought of such a sale, but this month has zoomed by me. So, since it is so late in the month, here is the *Tube CAD Journal's* Get Ready for New Year's sale:

From December 20, 2004 to January 1, 2005, all TCJ downloads will be on sale:

TCJ Push-Pull Calculator Download for only \$19	Save \$10
TCJ My-Stock DB Download for only \$14.95	Save \$5
TCJ Filter Designer Download for only \$9.95	Save \$3

Sorry to the stocking stuffers out there, but this sale applies only to downloads, not CDs, as I cannot imagine going to the Post Office this month.

01 January 2005

## The Perfect Line Amplifier & Perfect Reflections

### Subject: Aikido Amplifiers

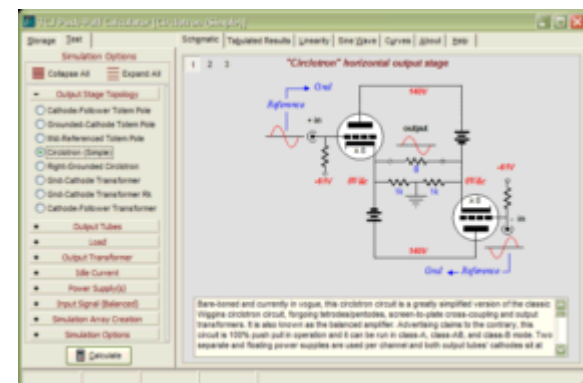
I must say that your Tube CAD Journal is most intriguing. You must be a very good chess player—bold and subtle at once. I appreciate the Aikido amplifier series of blogs (such and ugly word). But I wonder if it is the best route to hi fi. It puts out existing fires quite nicely, but why have any fires?

Attached is my line amplifier schematic. It is the perfect [line] amplifier as the constant current sources keep all power supply noise out and allow the triodes to perform perfectly. Constant current = no distortion. Removing the coupling capacitor makes the amplifier much purer sounding. (I have done many tests.)

My friends are amazed that my first attempt at designing tube circuit should

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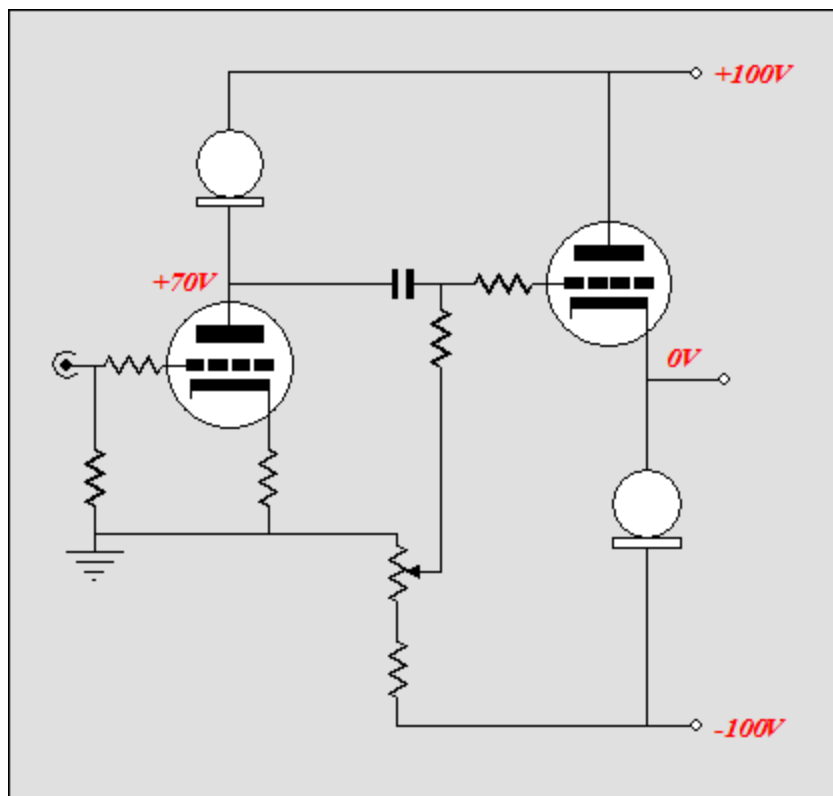
TCJ Push-Pull Calculator  
Version 2



be so perfect. Feel free to show schematic—no trade secrets here ;)

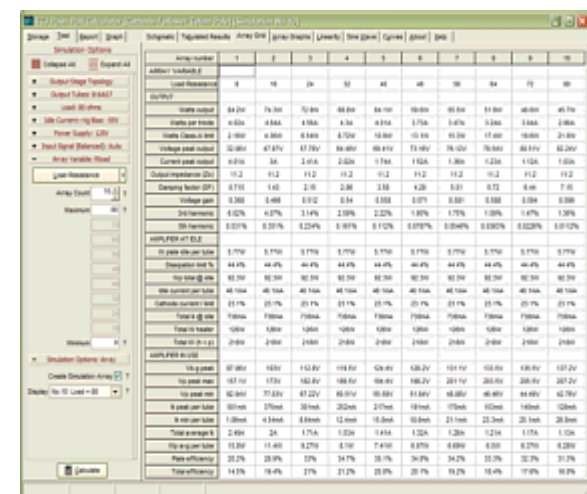
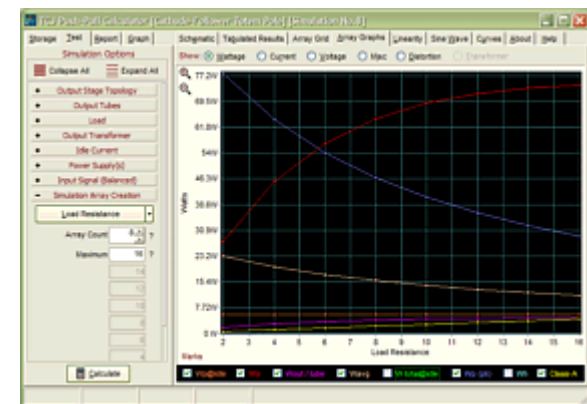
Carlo G.  
Italy

Carlo, thanks for the kind words. But I don't think I am half as bold as you, as I would be terrified to use the word "perfect." Yes, you are right: the Aikido approach works to undo what is already wrong and it would offer little in a perfect world, much as the real Aikido would be needless. (Yes, I know that there is a great deal more to Aikido than just self defense, but the "great deal more" would already be included if it were a truly perfect world; think about it.) As for chess, I love it, but I haven't played a game in 20 years. (I believe my style was closer to reckless and sneaky, but maybe I flatter myself. I was much moved by Paul Morphy's games) Now, for the good and bad news.

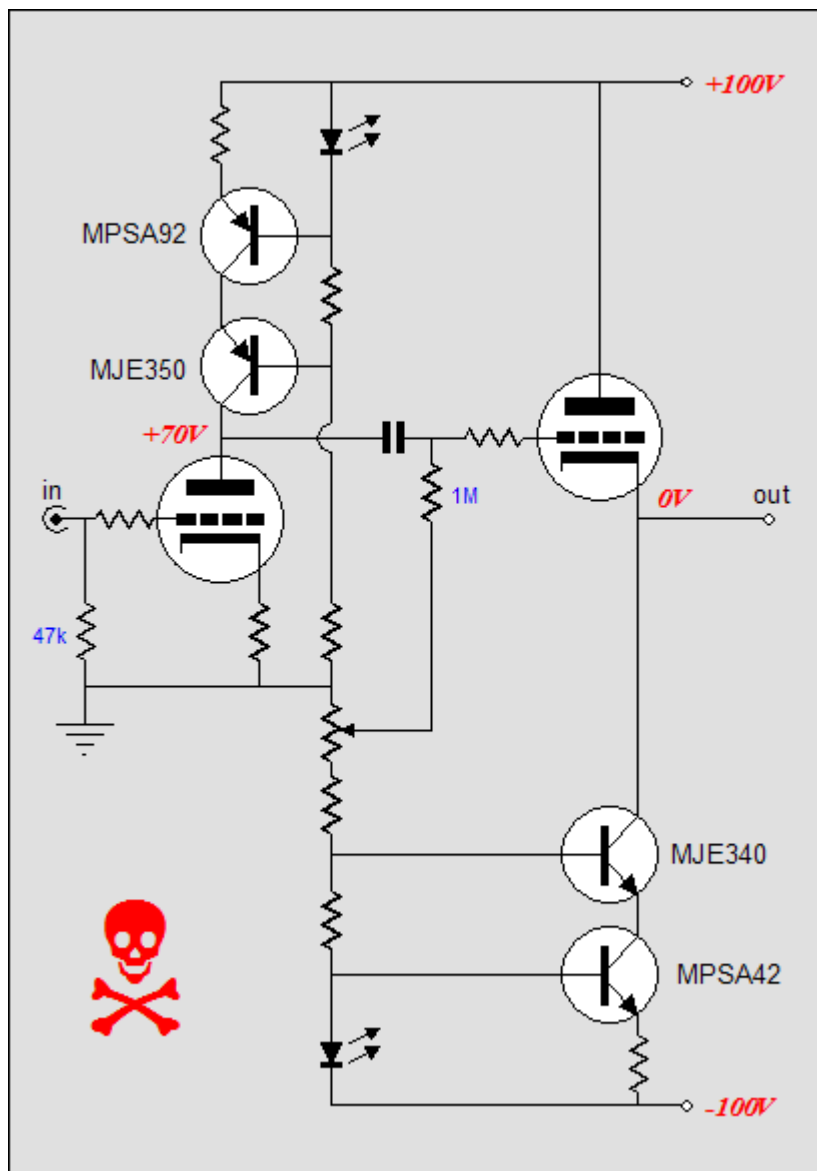


Above a quick overview of Carlo's Perfect Amplifier. The constant-current source loads the input triode, isolating the triode from the positive power supply rail's noise. It also allows the greatest gain from the triode (close to the amplification factor). And it also keeps the distortion low, although not nonexistent. (Draw a horizontal line across a set of plate curve and mark the distance between grid-line intersections. If there were no distortion, then the distances would be identical; they aren't.)

At the output, the constant-current source that loads the cathode follower does wonderful things for this buffer. It allows the greatest gain from the cathode follower and it buffers the cathode follower from the negative power supply noise. However, it does not lower the cathode follower's output impedance or make the cathode follower perfectly noise free. But



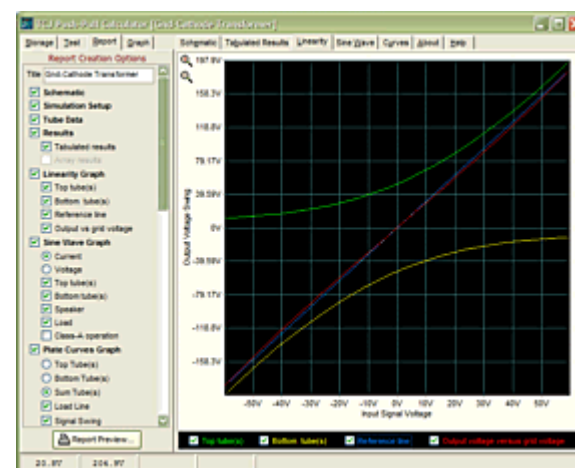
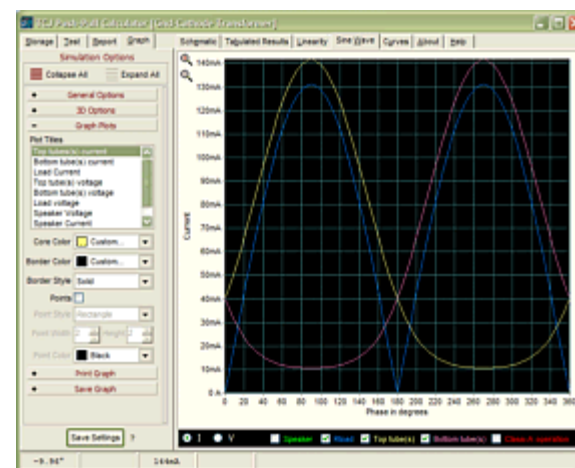
first, let's look at his complete schematic. (I took the liberty of adding grid-stopper resistors. If you think that grid-stopper resistors are a bad idea, try driving your car without shock absorbers, as they perform an analogous function: they add resistance to a dangerously reactive mix.)



The Perfect line amplifier

Carlo is not afraid of solid-state parts, which I think is healthy. (Imagine a biblical scholar who refused to learn Greek, relying exclusively on Hebrew to understand original New Testament manuscripts. Well, refusing to study solid-state—or vacuum state electronics—would be equally foolish.) The LEDs work as cheap voltage references (real voltage references—IC precision voltage references—are only a few dimes more, so why not use them?). All the transistors are high-voltage (the inner transistors are protected from the high-voltages by the MJE340 and MJE350, so why not use low-voltage transistors instead, particularly low-voltage, low noise transistors?)

The negative power supply matches the positive in voltage magnitude. The output is DC coupled and its offset is adjusted by the potentiometer.



## TCJ PPC Version 2 Improvements

- Rebuilt simulation engine
- Create reports as PDFs\*
- More Graphs 2D/3D\*
- Help system added
- Target idle current feature
- Redesigned array creation
- Transformer primary & secondary
- RDC inclusion
- Save user-defined transformer definitions
- Enhanced result display
- Added array result grid

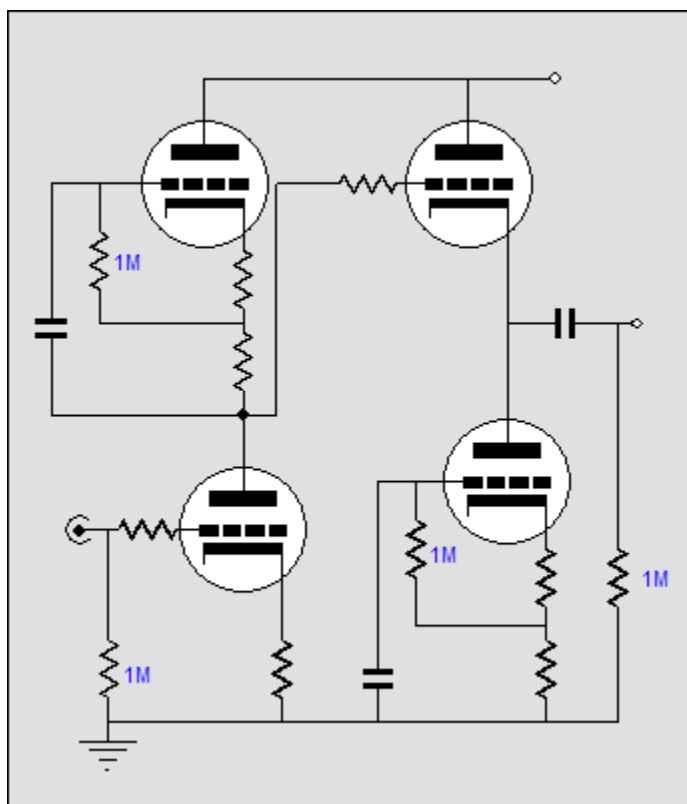
\*User definable

TCJ Push-Pull Calculator has but a single purpose: to evaluate tube-based output stages by simulating eight topologies' (five OTL and three transformer-coupled) actual performance with a specified tube, power supply and bias voltage, and load impedance. The accuracy of the simulation depends on the accuracy of the tube models used and the tube math model is the same True Curves™ model used in

All in all, not a bad line amplifier by any means (certainly better than many commercial efforts). Now for the *but*...but is it really coupling-capacitor free, when a coupling capacitor bridges the input stage to the cathode follower? If the amplifier which follows is a tube design, this might pose no problems, but what happens when a solid-state amplifier is used? For example, at startup, when the cathodes are cold, the solid-state constant-current sources are not dormant, but instantly excited to conduct their preset current. Thus, the solid-state amplifier will see its input swing  $-100$  volts (never a good idea). The cathode follower will see its grid swing  $+100$  volts, while its cathode sits at  $-100$  volts (quite a voltage differential for any tube). The same holds true for when a tube is jiggled in its socket.

**Do not use this circuit unless you know that it cannot harm your system; In other words, not recommended without a coupling capacitor at the output.**

Having said that, the goals are still admirable. A completely-tube-filled design would look like this:



The coupling capacitor has been restored to the output and triodes are used to create constant-current sources and the bipolar power supply has been reduced to a single polarity. This version is much safer than the original, but it also suffers from a power supply noise failing that a little Aikido can remedy.

Imagine that the first constant-current source works perfectly and the input stage is perfectly noise free. Now, this means that the cathode follower's triode sees at its grid zero noise, effectively ground, but its plate sees the full

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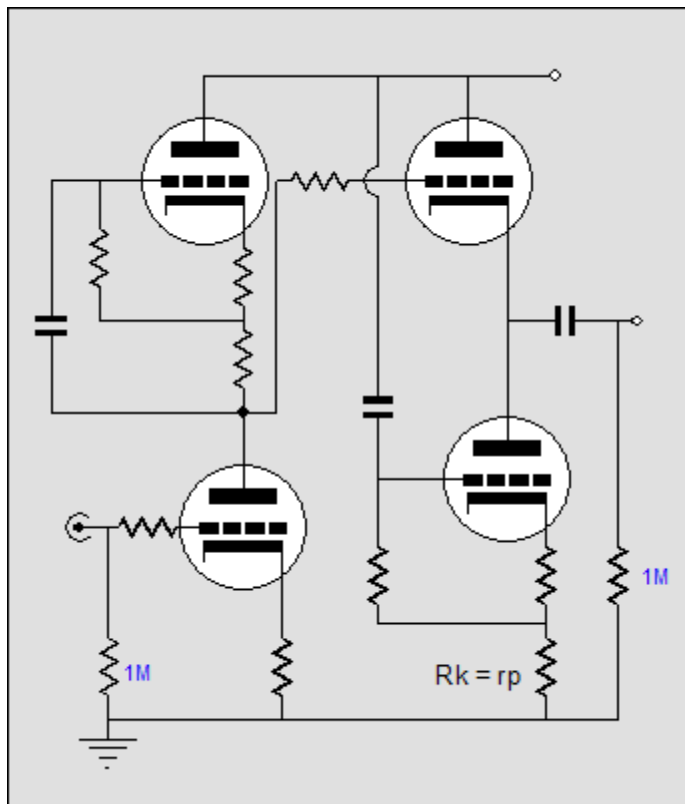
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magnitude of power supply noise. So what is the result at its cathode? Zero noise? Some noise?

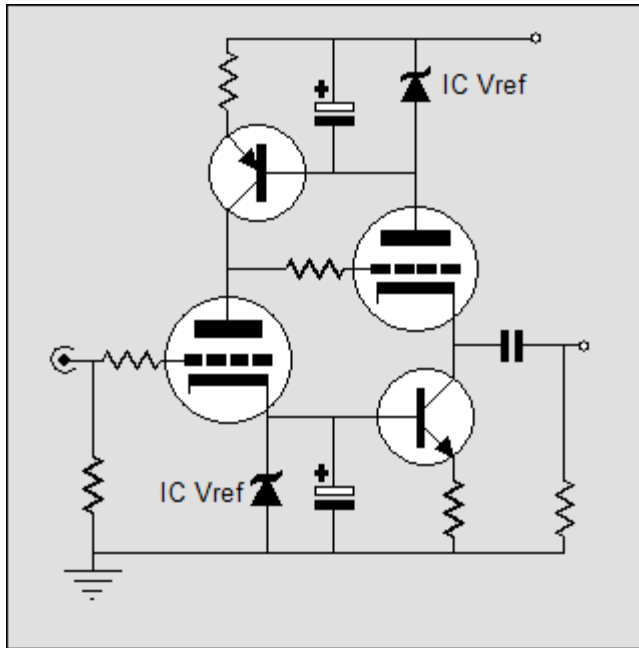
The answer is that the constant-current source only made the situation slightly worse, as the noise at the cathode can now approach its theoretical maximum of  $1/\mu$ . Think about it: the plate voltage varies, but the current flow is constant, as is the ground voltage. So the only thing that can vary (and something must vary) is the cathode voltage, as a triode can not conduct the same current with two sets of plate voltages and a constant ground voltage.

Thus, the need for a little Aikido. If the constant-current source that loads the cathode follower were to break its consistency enough to allow a little power supply noise, then the cathode could remain noise free, as its current conduction would no longer be constant. Ironic, isn't it?

The first step is to specify a bottommost cathode resistor equal to the triode's  $r_p$ . The next step is to "ground" the cathode follower's constant-current source at the B+ connection, not ground. What we have created here is a grounded-cathode amplifier that has a gain of  $1/\mu$  when loaded by the top tube's cathode impedance. Because the grounded-cathode amplifier inverts its input signal, the weakly amplified noise will cancel the weak amount of noise the top triode passes.



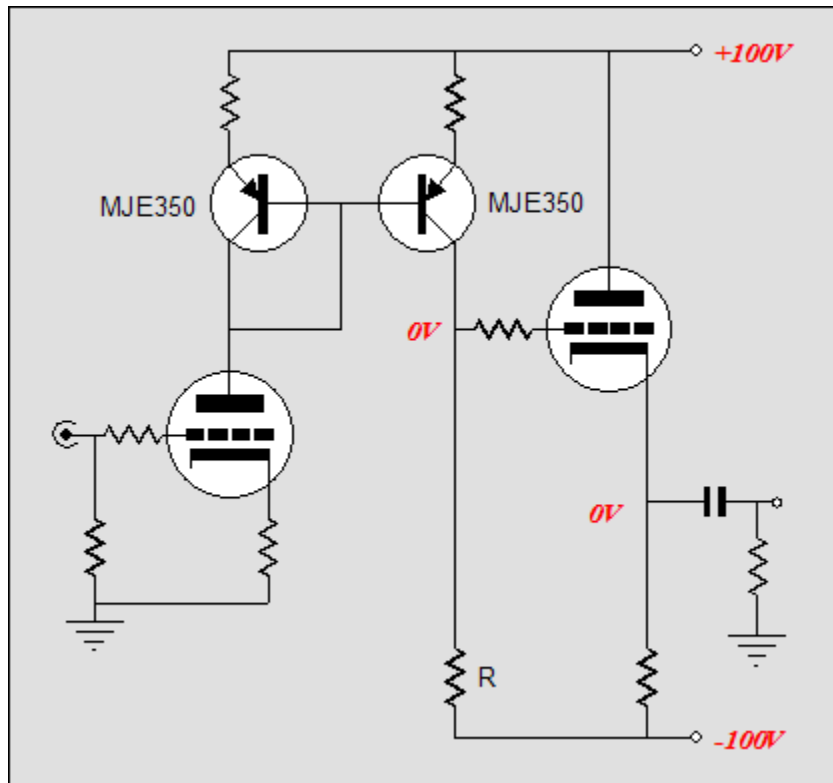
"Wait a minute," you say, "I use a regulated power supply, so I don't care about power supply noise; I just want super linearity." Well, if that's the case, why not use a "super" simpler circuit:



Once again two constant-current sources are employed and at the same places, but only two transistors are needed and high-quality voltage references are used instead of LEDs, which have always given me pause—I am not sure that I trust them.

### Current mirror rescue

Of course, the preceding circuit will not work with a bipolar power supply, such as Carlo uses. So, how can we take advantage of the negative rail? Well, since we are licensed to use solid-state devices, let's use a transistor-based current mirror. The current mirror samples the current flowing through the input triode and reflects an identical current draw from its output, which in this circuit, is terminated into a large valued resistor that is "grounded" into the negative power supply rail. Effectively, the current mirror has folded the current path on itself. The triode realizes its gain not at its plate, but at this load resistor.



The gain is roughly equal to what the triode would yield in a cascode circuit. With a bypassed cathode resistor, roughly,  $g_m \cdot R$ . Without a bypassed cathode resistor, roughly,

$$\mu \cdot R / (\mu + 1) R_k + r_p.$$

The cathode follower takes its input signal from this resistor's connection to the current mirror and it buffers it from the output. The cathode follower is not constant-current source loaded; purposely. First of all, I believe that constant-current source loading of a cathode follower is grossly oversold. Sure it looks great on paper, but in the real world where low-impedances abound, it makes little difference. For example, a 300-ohm headphone element in parallel with infinity is still 300 ohms, a tough load for any triode-based cathode follower.

But notice the noise relationships in this topology. The input tube sees almost all of the power supply noise at its plate, which induces a current variation roughly equal to

$$V_{\text{noise}} / (r_p + [\mu + 1] R_k).$$

This current variation is then transferred to the current mirror's output and develops a noise voltage equal to

$$R \cdot V_{\text{noise}} / (r_p + [\mu + 1] R_k).$$

But the connection to resistor R was not noise free to start with, as negative power supply rail holds a noise signal equal  $-V_{\text{noise}}$ . Thus, the final noise signal found at the top of resistor R is equal to

$$R \cdot V_{\text{noise}} / (r_p + [\mu + 1]R_k) - V_{\text{noise}}.$$

Well, if we specify that R equal  $r_p + (\mu + 1)R_k$ , then the equation reduces to

$$R \cdot V_{\text{noise}} / R - V_{\text{noise}}$$

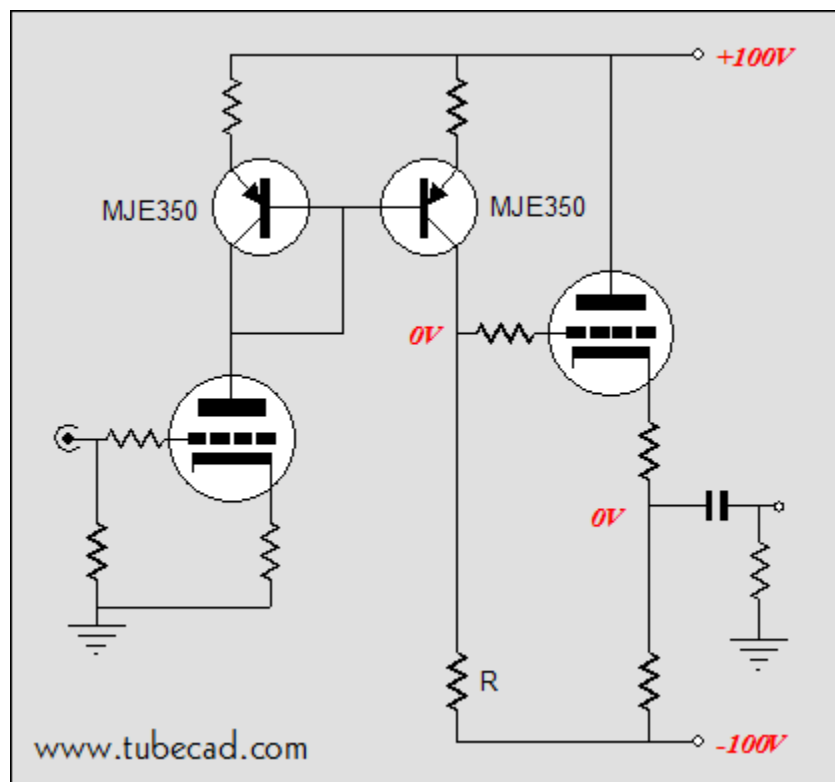
and then to

$$V_{\text{noise}} - V_{\text{noise}}.$$

Yes, zero. Ah, math...you have to love it.

So we have a noise-free input for the cathode follower, what about the noise leaving the cathode follower? Since the cathode follower is loaded by a cathode resistor equal to its  $r_p$ , both the triode and resistor experience the same noise current, which means that at their junction  $+V_{\text{noise}}$  cancels with  $-V_{\text{noise}}$ . Once again, zero.

The problem here is that since both triode and resistor see the same voltage differential, the triode's grid and cathode must share the same DC voltage, not a good idea. The solution requires one extra resistor.



Perfect Reflection line amplifier

The added cathode resistor combined with the triode define an effective “resistor” equal to  $r_p + (\mu + 1)$ . Now, we specify that the bottom cathode resistor equal this value as well. This way we retain the noise null and lighten the idle current through the cathode follower. Additionally, the amplifier out does not directly attach at the cathode. This is a secret way of



improving the sound, as the top cathode resistor buffers the cathode from the output (imagine 20 feet of high-capacitance cable) and linearizes the cathode follower's output.

## Conclusion

So, is this another perfect line amplifier? No, just a good line amplifier; in fact the Perfect Reflection line amplifier. (Remember, without a name, a topology doesn't exist.) Besides from a great PSRR figure, this amplifier offers an extremely low input capacitance, as the Miller-effect capacitance does not obtain, as the plate does amplify the input signal.

## PS

We specified that resistor R equal  $r_p + (\mu + 1)R_k$ , but that was a rough approximation and the complete equation is a bit thicker, but not by much:

$$R = r_p + (\mu + 1)R_k + R_{cm},$$

Where  $R_{cm}$  equals the current mirror's resistor into which the input triode terminates.

//JRB

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