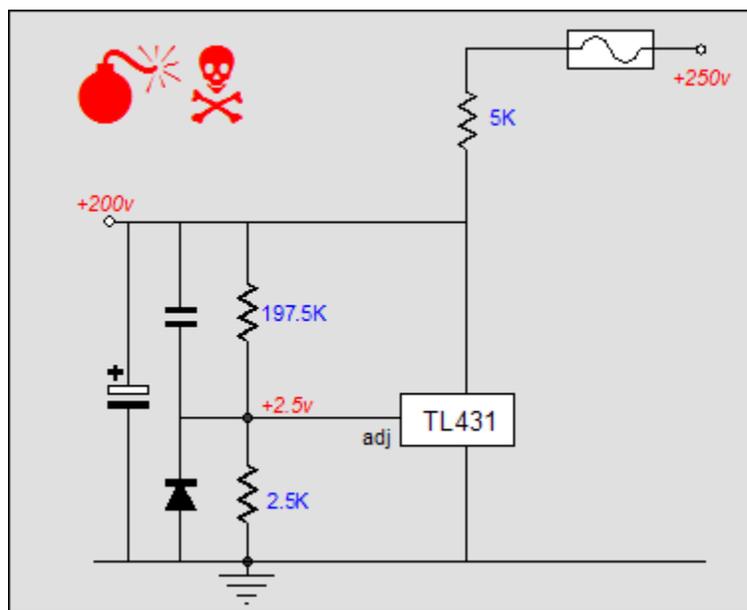
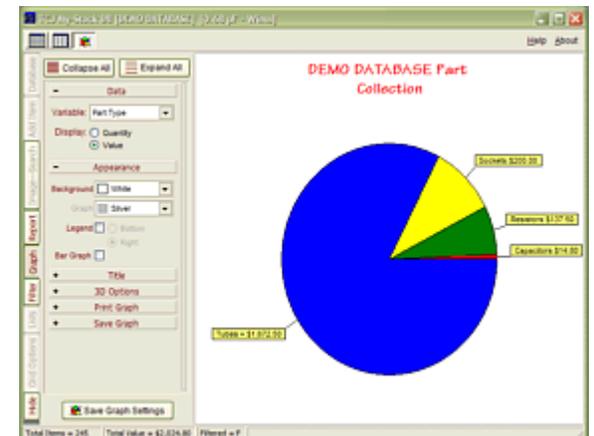
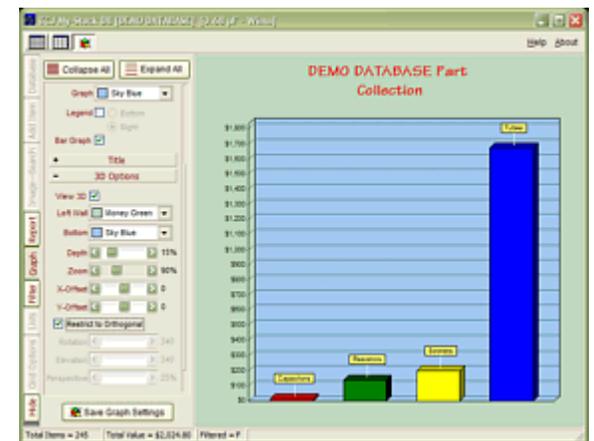


The only problem is—albeit a small problem, but a problem nonetheless—the schematic above is the TL431's internal schematic. As great as the TL431 might be, many ask too much of it, either demanding it withstand too much voltage or draw too much current. The TL431 can only withstand 36 volts, so the circuit below is definitely a bad idea.



The TL431 can only source up to 100mA, so the circuit below is equally a bad idea.



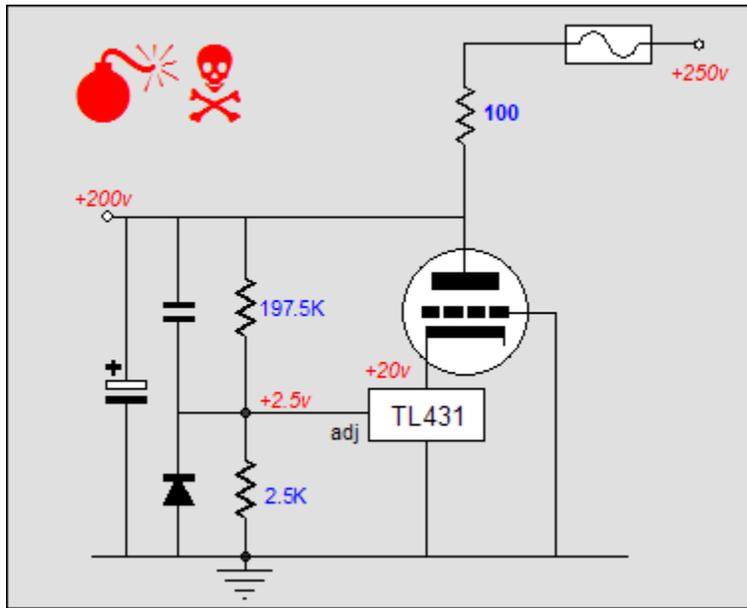
Part Type	Name	Quantity	Brand	Vendor
Tube	2A3	3	RCA	Electronic Parts
Tube	6BL7	4	Sylvania	Swap Me
Amp	6812	4	Sylvania	Jera's TV & S
Tube	6SL7	11	Tung-Sol	Jera's TV & S
Diode	1N4148	3	Deflection	Free Mart
Tube	6SL7	18	Sylvania	Free Mart
Tube	12AT7	22	National	Swap Me
Tube	5687	6	Tung-Sol	Swap Me
Tube	6BD6A	4	GE	Antique Electron
Tube	5891	3	RCA	Swap Me
Tube	6L84	5	Mullard	Swap Me

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Absolute Maximum Ratings

(Operating temperature range applies unless otherwise specified.)

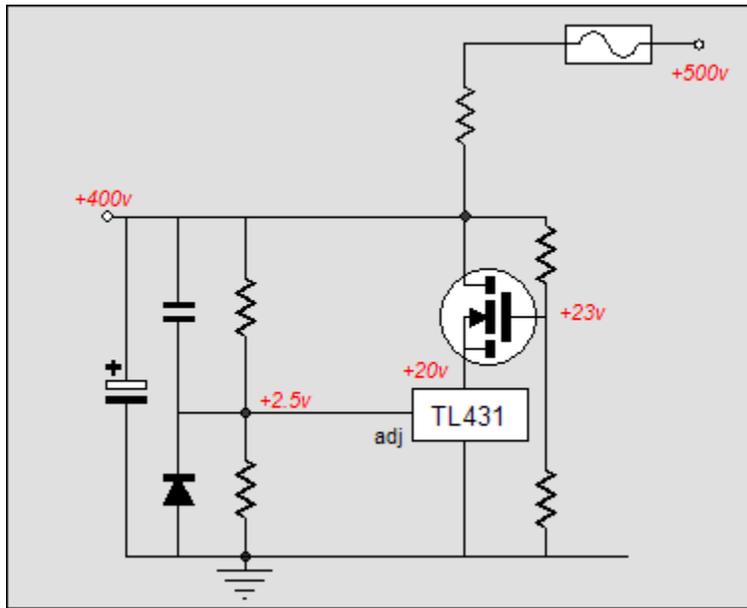
Parameter	Symbol	Value	Unit
Cathode Voltage	VKA	37	V
Cathode Current Range (Continuous)	IKA	-100 ~ +150	mA
Reference Input Current Range	IREF	-0.05 ~ +10	mA
Power Dissipation D, LP Suffix Package P Suffix Package	PD	770 1000	mW mW
Operating Temperature Range	TOPR	-25 ~ +85	°C
Junction Temperature	TJ	150	°C
Storage Temperature Range	TSTG	-65 ~ +150	°C

Recommended Operating Conditions

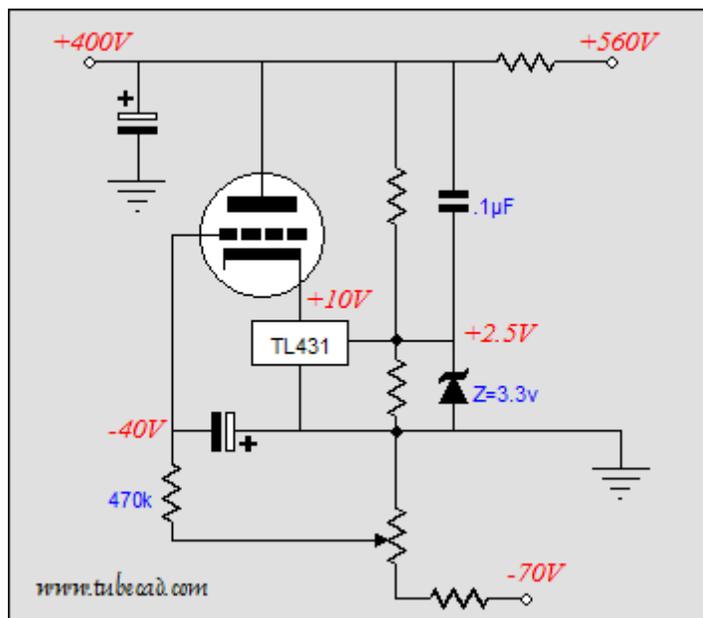
Parameter	Symbol	Min	Typ	Max	Unit
Cathode Voltage	VKA	VREF	-	36	V
Cathode Current	IKA	1.0	-	100	mA

The above table was lifted from the Fairchild TL431A PDF and it lists the limits within which the device will operate. Note, the TL431 cannot see 36 volts across its leads and draw 100mA at the same time, as that would result in 3.6 watts of dissipation, far more than the 770mW that it can withstand. (Also note that 770mW limit is at a cool 30 c and must be derated for higher temperatures.)

Extending the TL431's voltage limit is easy enough, as we can cascode the TL431 with either a tube or a transistor or a MOSFET (placing a zener in series with it is neither safe nor desirable). Above we saw a tube sitting atop the TL431; below, a high-voltage MOSFET.

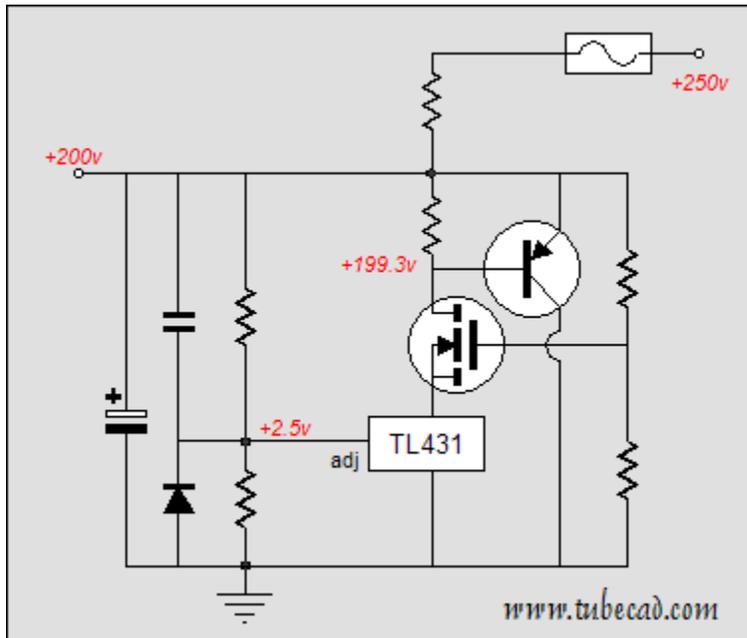


The potential problem with the tube-based hybrid shunt regulator is that at turn-on the tube's cathode is cold and not conducting, which means no voltage regulator until it is hot. Second, the triode might require a much larger negative bias voltage than the TL431's 36 volt limit. The workaround is to use a negative power supply connection to help bias the triode.

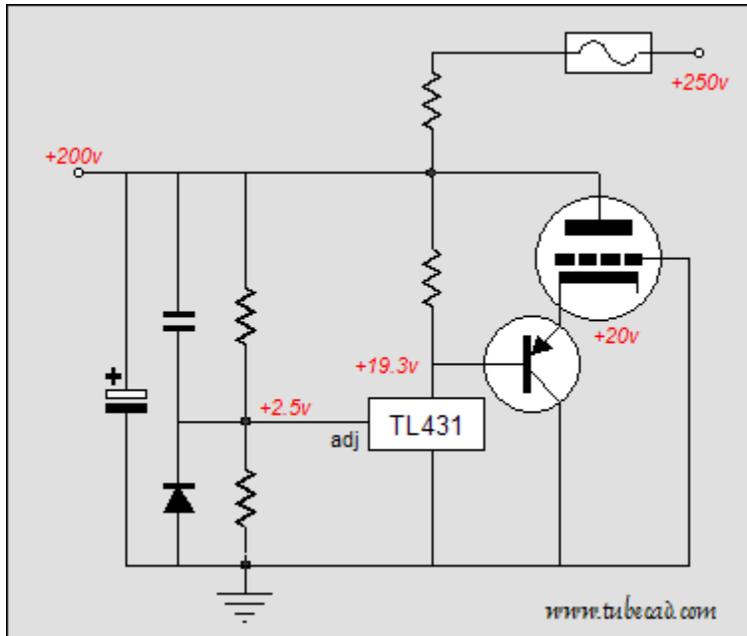


Here the triode sees a -50 volts grid-to-cathode bias voltage, while the TL431 only sees a 10 volt differential. (The optimal anode-to-cathode voltage for the TL431 would equal $(36V - 2.5V) / 2 + 2.5V$, as it would allow the greatest cathode swing on the TL431.)

Increasing the current capability of the TL431 is also easily accomplished with more parts.)



Or



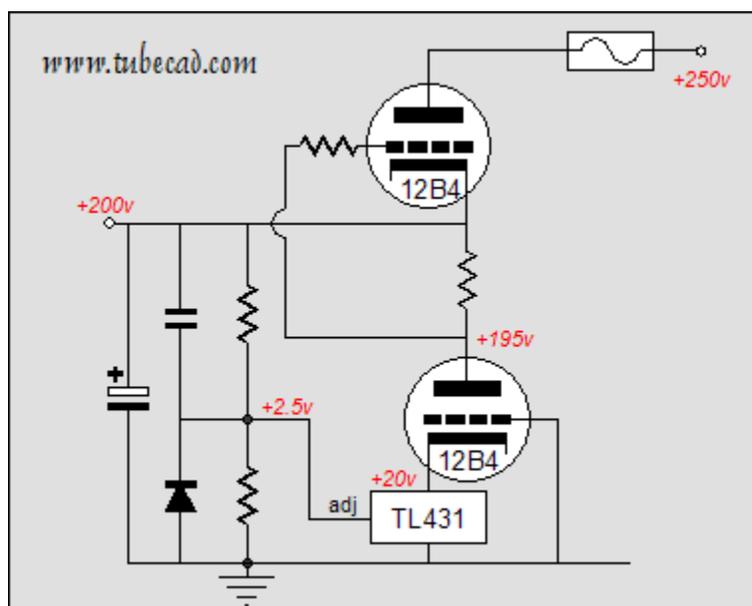
One common mistake is to ask the control element of a shunt regulator (the TL431 in this case) to draw too much current. For example, let's say you have a phono preamp that draws a total of 40mA, How much current should the TL431 draw? 90% of readers will answer 40mA, but in fact, much less is needed. Consider this: the preamp only puts 1V of output signal, which into a 100K potentiometer only equals 0.01mA of current variation.

If the load draws a fairly steady current, as single ended circuits and class-A output stages tend to do, then the shunt regulator need only make up the delta in current draw between minimum and maximum, plus whatever wall voltage fluctuations that must be compensated. In other words, 40mA is way too much current, as a total (shunt regulator and load) current draw of 60mA would probably be more than sufficient.

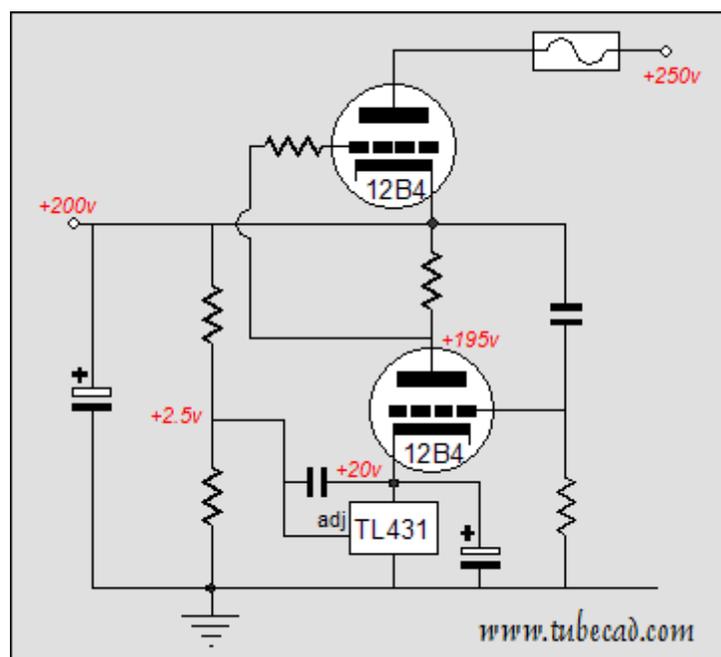
SRPP shunt regulators

Here's a circuit to ponder: an SRPP shunt regulator. The TL431 is cascaded

with a 12B4 triode, which in turn drives another 12B4. This regulator can source and sink current, as it comprises a shunt and series regulator.

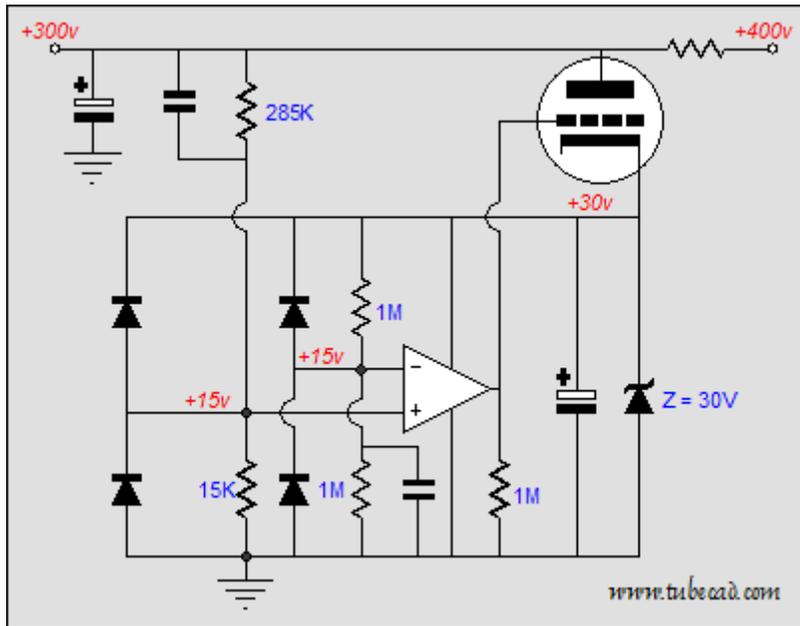


For some, the thought of letting a IC control the output of the shunt regulator is as scary as letting a IC control the sound coming out of a tube amplifier. The circuit below uses the TL431 to adjust the DC output voltage of the regulator, while the 12B4s control the AC output of the regulator.



TL431-less shunt regulator

What if all the TL431's internal functions were handled by discrete devices, devices that exhibited much higher performance? Such a circuit would look much like the one below.



//JRB

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